

ELECTRODE-LESS FERRITE-FREE CLOSED-LOOP INDUCTIVELY-COUPLED FLUORESCENT LAMP

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ABSTRACT

Electrode-less ferrite-free inductively-coupled low pressure discharge was excited in the mixture of mercury vapour ($\sim 10^{-2}$ Torr) and argon (0.1 Torr) at a frequency of 2.0 MHz and lamp *RF* powers of (150–202) W with the help of a 6-turn induction coil. The discharge lamp of rectangular shape (50 cm in length and 7 cm in height) employed a closed-loop glass tube of 30 mm in diam. Tube walls inner surface was coated with three-color phosphor ($T_{cc} = 3100$ K, $R_a = 80$). The induction coil made from silver-coated copper wire ($\rho_w = 2.2 \times 10^{-3}$ Ohm/cm) was disposed on the atmospheric side of tube walls, along closed-loop lamp tube perimeter. As plasma power, P_{pl} , grew from 127 W to 180 W, coil power losses practically were unchanged, $P_{coil} = (25-22)$ W. Lamp luminous flux, Φ_v , grew with plasma power from 10430 lm ($P_{pl} = 127$ W) to 13500 lm ($P_{pl} = 180$ W), while plasma efficacy, $\eta_{pl} = \Phi_v/P_{pl}$, decreased from 82 to 75 lm/W, and lamp efficacy $\eta_V = \Phi_v/(P_{pl} + P_{coil})$ decreased from 70 to 67 lm/W.

Keywords: ferrite-free inductive discharge, fluorescent lamp, low pressure mercury plasma, coil power losses, lamp and plasma efficacy, radiofrequency voltage (*RF*)

1. INTRODUCTION

Transformer-type inductively-coupled light sources excited in the mixture of low pressure mercury vapour and inert gas at *RF* frequencies (0.1–13.56) MHz and *RF* power (50–500) W have

shown excellent characteristics: high luminous efficacy (up to 100 lm/W) and very high life-time (> 60000 h) [1, 2]. However, transformer-type lamp has one but substantial disadvantage: expensive and fragile ferrite cores encircling a closed-loop discharge tube. Meanwhile, ferrite-free inductively-coupled discharges could be excited at *RF* frequencies in a closed-loop lamp made from a tube of (50–70) mm in diameter with the help of an induction coil disposed on the atmospheric side of lamp walls, along its “inner” perimeter [3].

Here, we present results of an experimental study of ferrite-free closed-loop inductively-coupled lamp employing discharge tube of 30 mm in diameter excited with the help of an induction coil encircling the lamp around its “outer” perimeter.

2. EXPERIMENTAL SET-UP AND MEASUREMENT TECHNIQUES

An inductive plasma was excited and maintained at a frequency $f = 2.0$ MHz and *RF* power of $P_{pl} = (127-180)$ W in the mixture of mercury vapour and argon in a closed-loop lamp made from cylindrical glass tube of 30 mm in diam. Tube walls inner (vacuum) surface was coated with three-colour phosphors ($T_{cc} = 3100$ K, $R_a = 80$). The lamp has rectangular shape of 500 mm in length and of 70 mm in height; the distance between two discharge tubes was $H_2 = 6$ mm (Fig. 1). A 6-turn induction coil made from silver-coated copper wire ($\rho_w = 2.2 \times 10^{-3}$ Ohm/cm) encircled the closed-loop discharge lamp along its perimeter. Mercury vapour was maintained at optimum pressure of $\sim 10^{-2}$ Torr by con-

trolling amalgam (Bi-In-Hg) temperature; argon pressure was 0.1 Torr.

Sinusoidal RF voltage at a frequency of 2,0 MHz was sent from the signal generator (PM 5193, Philips) to the wideband amplifier (A-300, ENI), and further to the directional coupler (C5100, Werlatone). Forward and reflected RF power, P_{for} and P_{ref} , were measured with the help of RF power meter (NAP Z8, Rhode-Schwartz). The transferred RF power $P_{tr} = P_{for} - P_{ref}$ comprised plasma absorbed power, P_{pl} , induction coil power losses, P_{coil} , and RF power P_{cap} dissipated in low loss (<1 W) matching network ceramic capacitors C_{ser} and C_{par} . Induction coil RF voltage and current, U_c and I_c , phase shift between them, φ , and lamp and matching network powers, P_{lamp} and P_{cap} , were measured with the help of high voltage probe, current transformer, and 4-channel oscilloscope HP 54503A. Lamp luminous flux, Φ_v , spectrum, and lamp colour characteristics, T_{cc} and R_a were measured with the help of the computerized photometrical sphere. Plasma and lamp efficacy were calculated as $\eta_{pl} = \Phi_v/P_{pl}$, and $\eta_v = \Phi_v/P_{lamp} = \Phi_v/(P_{pl} + P_{coil})$, respectively.

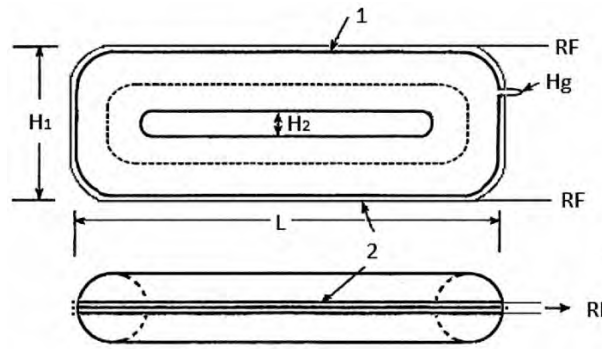


Fig. 1. Schematic drawing of ferrite-free closed-loop inductively-coupled lamp: 1 – discharge tube; 2 – induction coil; Hg – exhaust tubing with amalgam; RF – radio-frequency voltage

2. EXPERIMENTAL RESULTS AND DISCUSSION

The results of measurements are shown in Figs. 2, 3. It is seen from Fig. 2 that coil power losses, P_{coil} , did not show dependence from plasma power, P_{pl} , and had values of (22–25) W. Lamp luminous flux, Φ_v , grew as plasma power increased from 10430 lm ($P_{pl} = 127$ W) to 13500 lm ($P_{pl} = 180$ W). Coil power efficiency $\eta_c = 1 - P_{coil}/(P_{pl} + P_{coil})$ increased with plasma power from 0,85 ($P_{pl} = 127$ W) to 0,89 ($P_{pl} = 180$ W), while lamp and plasma efficacies, η_v and η_{pl} , decreased from 70 to 67 lm/W, and from 82 to 75 lm/W, respectively (Fig. 3). The decrease of plasma efficacy η_{pl} as plasma power grew was due to the growth of the frequency of quenching collisions of resonantly excited mercury atoms with plasma electrons [3, 4].

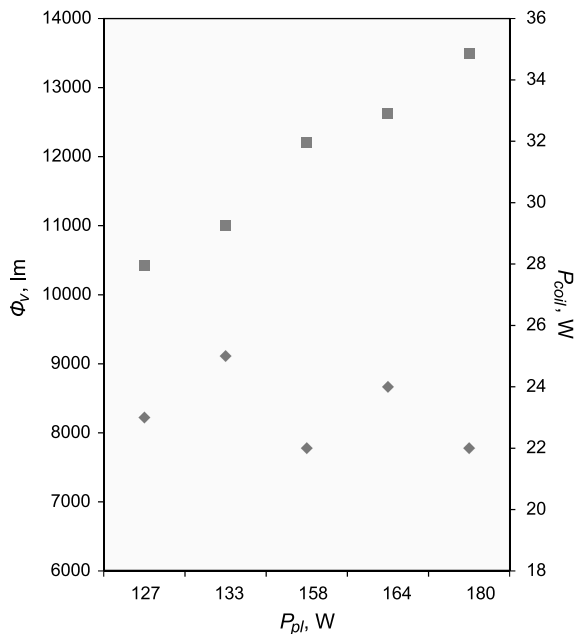


Fig. 2. Lamp luminous flux, Φ_v , and induction coil power losses, P_{coil} , as functions of plasma power, P_{pl} . ■ – Φ_v ; ♦ – P_{coil}

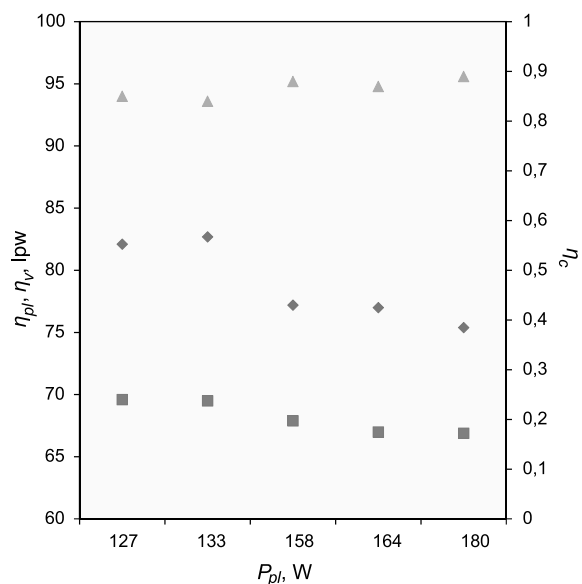


Fig. 3. Lamp and plasma efficacies, η_v and η_{pl} , and induction coil power efficiency, η_c , as functions of plasma power, P_{pl} . ♦ – η_{pl} ; ■ – η_v ; ▲ – η_c

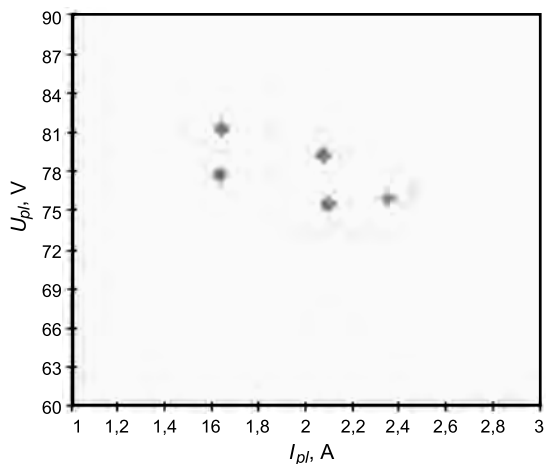


Fig. 4. Lamp volt-ampere characteristic, U_{pl} vs I_{pl}

Discharge current, I_{pl} , calculated within the framework of inductive discharge transformer model grew with plasma power from 1.63 A ($P_{pl} = 127$ W) to 2.35 A ($P_{pl} = 180$ W). While RF electric field, \bar{E}_{pl} , averaged across plasma diameter, decreased insignificantly from 0.76 to 0.72 V/cm. These values are essentially the same as RF electric fields ($E_{pl} = (0.73\text{--}0.78)$ V/cm) in the transformer lamp plasma excited in mixture of mercury vapour ($\sim 10^{-2}$ Torr) and argon (0.1–0.12 Torr) in the closed-loop tube of 16.6 mm in diam. at a frequency of $f = 265$ kHz and plasma power of $P_{pl} = 180$ W [5]. The dependence of plasma RF voltage, U_{pl} , from discharge current, I_{pl} , plotted in Fig. 4 has negative character and is in good agreement with the dependence of \bar{E}_{pl} from P_{pl} that is typical for high density low pressure mercury discharges [4].

3. CONCLUSION

It was experimentally shown that plasma efficacy 80 lm/W and lamp efficacy 70 lm/W could be obtained in a ferrite-free closed-loop inductively-coupled mercury low pressure fluorescent lamp with discharge tube of 30 mm in diam. The further increase of plasma efficacy η_{pl} could be achieved by rising argon pressure to (0.2–0.3) Torr, at which ultraviolet UV ($\lambda = 254$ nm) radiation generation in the inductive discharge in the closed-loop lamp with tube of 16,6 mm in diameter operated at the same power level was found to be maximal [5]. To substantially increase lamp efficacy, $\eta_V = \eta_c \eta_{pl}$, induction coil efficiency, η_c , should be increased to 0,95–0,97 by reducing coil power losses to (4–5) W. This could be done by using in induction coil low loss ($\rho_w \leq 5 \times 10^{-4}$ Ohm/cm) Litz wire [3].

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